

ON A DIFFERENTIAL PRINCIPLE OF HIGHER ORDER  
FOR NON-HOLONOMIC MECHANICAL SYSTEMS

V. Čović

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1. In the case where the mechanical system is acted upon by ideal non-holonomic constraints of the most general form, a function is formed by applying the Gauss function of constraint, the variation of this function, in virtue of the principle of  $m$ -th order, being equal to zero. Equations of motion of the mechanical system under consideration were also obtained.

2. The differential principle of the  $m$ -th order\*

$$\sum_{i=1}^N (m_i \vec{r}_i - \vec{F}_i) \delta_m \vec{r}_i = 0,$$

where

$$\vec{r}_i = \vec{r}_i(q^1, \dots, q^n), \quad n = 3N,$$

$$\vec{r}_i = \frac{d^m \vec{r}_i}{dt^m}, \quad \delta_m \vec{r}_i = \delta \vec{r}_i (\delta \vec{r}_i = \delta \vec{r}_i = \dots = \delta \vec{r}_i = 0),$$

can be written also in the form of

$$\delta_m^{(m-2)} Z = 0, \quad Z = \frac{d^{m-2} Z}{dt^{m-2}},$$

or

$$(1) \quad \frac{\partial Z}{\partial q^K} \delta q^K = 0,$$

where  $Z$  is Gauss's function of constraint.

\* The indices take the following values:

$j, k, r, s = 1, \dots, n; \quad \mu = 1, \dots, p; \quad \nu, \rho = p+1, \dots, p+l = n.$

As shown in (2), we have

$$(2) \quad Z = \frac{1}{2} g_{Kr} (f^K - Q^K) (f^r - Q^r),$$

and, after introducing the Appell function of acceleration

$$S = \frac{1}{2} g_{Kp} f^K f^r,$$

and bearing in mind that

$$Z = S^{(m-2)} - Q_K^{(m-2)} q^K + \psi(q^j, \dot{q}^j, \dots, q^{(m-1)j}),$$

the expression (1) can be rewritten in the well known form of

$$(3) \quad \left( \frac{\partial S^{(m-2)}}{\partial q^K^{(m)}} - Q_K^{(m)} \right) \delta q^K^{(m)} = 0.$$

Provided the expressions for the Appell function and the kinetic energy of the system involved are written in the form of

$$S = \frac{1}{2} \underline{\underline{a}} \circ \underline{\underline{a}}, \quad T = \frac{1}{2} \underline{\underline{v}} \circ \underline{\underline{v}},$$

where

$$\underline{\underline{v}} = \dot{q}^k \underline{\underline{g}}_k, \quad \underline{\underline{a}} = f^k \underline{\underline{g}}_k, \quad g_{kr} = \underline{\underline{g}}_k \circ \underline{\underline{g}}_r,$$

then

$$T = \underline{\underline{v}} \circ \underline{\underline{v}}^{(m)} + \binom{m}{1} \underline{\underline{v}} \circ \dot{r}^{(m-1)} + \alpha(q^j, \dots, q^j)^{(m-1)},$$

$$S = \underline{\underline{a}} \circ \underline{\underline{a}}^{(m-2)} + \beta(q^j, \dots, q^j)^{(m-1)},$$

so that, because of

$$\frac{\partial}{\partial q^j} (\underline{\underline{v}} \circ \underline{\underline{v}})^{(m)} = (m+1) g_{rS} \Gamma_{jk}^r \dot{q}^k \dot{q}^S,$$

$$\frac{\partial S^{(m-2)}}{\partial q^j} = \frac{1}{m} \frac{\partial T}{\partial q^j} - \frac{m+1}{m} \frac{\partial T}{\partial q^j},$$

the expression (1) obtains its well known (3)

$$(4) \quad \left[ \frac{1}{m} \frac{\partial T}{\partial q^j} - \frac{m+1}{m} \frac{\partial T}{\partial q^j} - Q_j \right] \delta q^j = 0.$$

3. Let the system be subject to constraints of the most general form ([1], [3], [4])

$$\varphi^{\nu}(q^j, \dot{q}^j, \dots, q^{(m-1)j} t) = 0,$$

which can be rewritten in the following way, too,

$$\frac{\partial \varphi^{\nu}}{\partial q^j} \dot{q}^j + \frac{\partial \varphi^{\nu}}{\partial \dot{q}^j} \ddot{q}^j + \dots + \frac{\partial \varphi^{\nu}}{\partial q^{(m-1)j}} q^{(m-1)j} + \frac{\partial \varphi^{\nu}}{\partial t} = 0,$$

whence, in virtue of

$$\frac{\partial \varphi^{\nu}}{\partial q^{(m-1)j}} \delta q^{(m-1)j} = 0$$

we can write

$$\delta q^{\nu} = b_{\mu}^{\nu} \delta q^{\mu}, \quad b_{\mu}^{\nu} = b_{\mu}^{\nu}(q^j, \dot{q}^j, \dots, q^{(m-1)j}).$$

By taking into consideration the last equation, (1) can be given the form of

$$\delta_m^{(m-2)} Z = \left( \frac{\partial Z}{\partial q^{\mu}} + b_{\mu}^{\nu} \frac{\partial Z}{\partial q^{\nu}} \right) \delta q^{\mu} = 0,$$

where from there follow the equations of motion of the system under consideration:

$$\frac{\partial Z}{\partial q^{\mu}} + b_{\mu}^{\nu} \frac{\partial Z}{\partial q^{\nu}} = 0.$$

If

$$\det \left[ \frac{\partial \varphi^{\nu}}{\partial q^{\rho}} \right] \neq 0,$$

then it is possible to write

$$q^{\rho} = \psi^{\rho}(q^j, \dot{q}^j, \dots, q^{(m-1)j}, q^{\mu}, t)$$

so that it is quite obvious that

$$\psi^{\rho} = b_{\mu}^{\rho} q^{\mu} + \varphi^{\rho}(q^j, \dots, q^{(m-1)j}, t).$$

If we put

$$Z^* = Z(q^{\rho} = \psi^{\rho})$$

then the differential principle of the  $m$ -th order can be written in the form of

$$(5) \quad \delta_m^{(m-2)} Z^* = 0,$$



out of which there follow the equations of motion of the system involved,

$$(6) \quad \frac{\partial Z^{(m-2)*}}{\partial q^\mu} = 0,$$

or (see, also [5])

$$(7) \quad \frac{\partial S^{(m-2)*}}{\partial q^\mu} = Q_\mu + b_\mu^\rho Q_\rho,$$

where

$$S^{(m-2)*} = S^{(m-2)}(q^\rho = \psi^\rho).$$

For  $m=2$ , the equations (7) are transformed into so-called Appell's equations. It is obvious that the Appell equations are a direct consequence of the Gauss principle. In fact, Appell divided the Gauss function of constraint into three parts: the part which represented the quadratic form of variables  $\ddot{q}^j$  was designated by  $S$ ; the part which is the linear form of the variables  $\dot{q}^j$  provides the generalized force; and, finally, the third part was discarded since it is not subject to variations.

From the preceding expostulations, we can see that the Gauss function of constraint ( $z$ ) is a unique function in Analytical Mechanics with reference to the shortness of forms in which differential principles and equations of the mechanical systems are expressed.

4. In [4], the equations of motion of the mechanical system under consideration, that was subject to constraints

$$\dot{q}^\rho = a_\mu^\rho(q^1, \dots, q^n, t) \dot{q}^\mu + a^\rho(q^1, \dots, q^n, t)$$

were derived in the following way. The functions

$$K_m = \frac{1}{m} \left[ T^{(m)} - (m+1) \frac{\partial T^{(m)}}{\partial q^j} q^j \right] - Q_j q^j$$

and

$$(8) \quad K_m^* = K_m(q^\rho = a_\mu^\rho \dot{q}^\mu + \dots),$$

were first introduced, and then, from the condition of extremum of the function  $K_m^*$ , the differential equations of motion

$$(9) \quad \frac{\partial K_m^*}{\partial q^\mu} = 0.$$

were formed.

These equations are exact, but they are derived by wrong considerations. This is obvious if one bears in mind that

$$K_m = \mathcal{L}_s q^s + \dots, \quad L_s = \frac{d}{dt} \frac{\partial T}{\partial \dot{q}^s} - \frac{\partial T}{\partial q^s} - Q_s,$$

where in the expression for  $K_m$ , terms which were not important for the expressions (9), were omitted. By considering (8) and

$$L_s = g_{ks} \ddot{q}^k + \Gamma_{s,kr} \dot{q}^k \dot{q}^r - Q_s$$

it is quite obvious that  $K_m^*$  has its extremum only for  $m=2$ , and this is a well known fact. When  $m>2$ , the equations (8) are not proved by a correct method.

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#### SUR LE PRINCIPE DIFFERENTIEL D'ORDRE SUPERIEUR DES SYSTEMES NON-HOLONOMES

Vukman Čović

#### Résumé

On formule un principe d'ordre supérieur dont l'essentiel est que la variation de la fonction, formée à l'aide de la fonction de Gauss, est égal à zéro.



## О ДИФЕРЕНЦИЈАЛНОМ ПРИНЦИПУ ВИШЕГА РЕДА ЗА НЕХОЛОНОМНЕ МЕХАНИЧКЕ СИСТЕМЕ

*Вукман Човић*

### Резиме

У раду се разматра механички систем подвргнут дејству идеалних нехолономних веза.

Полази се од принципа  $m$ -тога реда који се, користећи Гаусову функцију најмање принуде, трансформише на облик (1). Даље се показује да су са (1) еквивалентни познати облици (3) и (4).

У случају да је механички систем подвргнут дејству идеалних нехолономних веза вишега реда, диференцијални принцип (1) може да се напише у форми (5), из које је очигледно да Гаусова функција најмање принуде омогућава да се једначине кретања разматраног нехолономног система изразе у најкондензованијем облику (6).

На крају дат је осврт на решење овог проблема и радовима [3] и [4]. Показано је да се у тим радовима садрже извесне непрецизности.

Vukman Čović  
Mašinski fakultet  
27. marta 80  
11 000 Beograd